

PL 4 - AC Motors - Main components

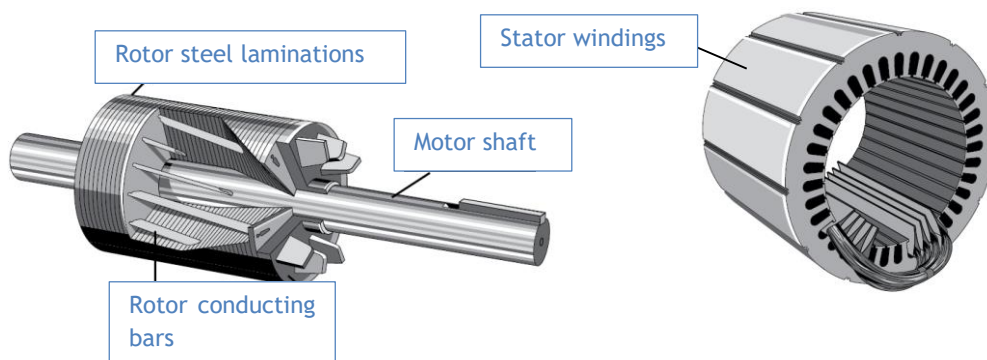
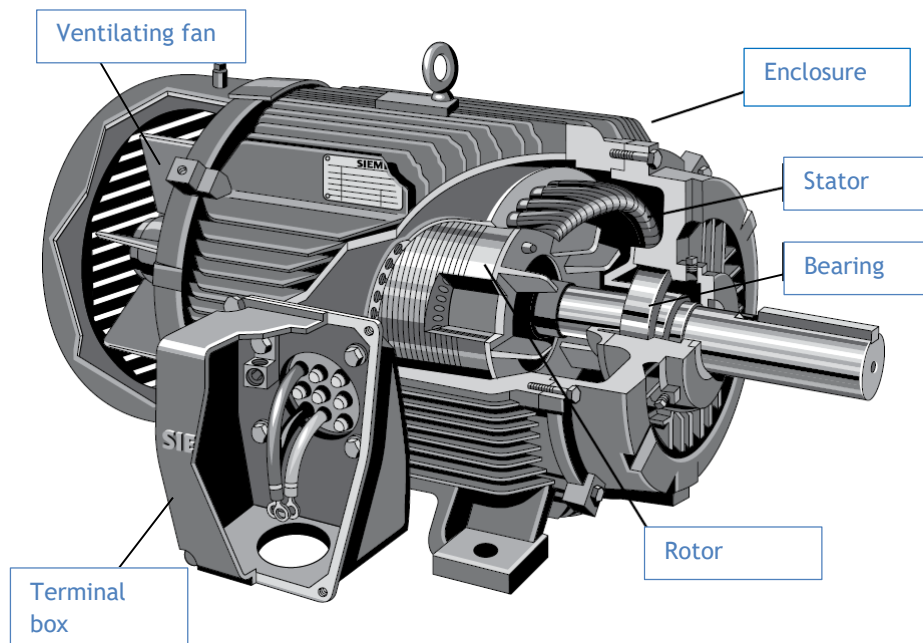
Objectives: Identification of the main components and demonstration of the working principle of induction (AC) motors (three phases and one phase). Characteristic curves (ex. Torque-speed). Three phases balanced electrical power, star (Y) and delta ( $\Delta$ ) connections.

Documents available

PL classes: 1) Catalogue carpanelli-M71b4.pdf

Web sites: [www.carpanelli.net](http://www.carpanelli.net)  
[www.marellimotori.com](http://www.marellimotori.com)

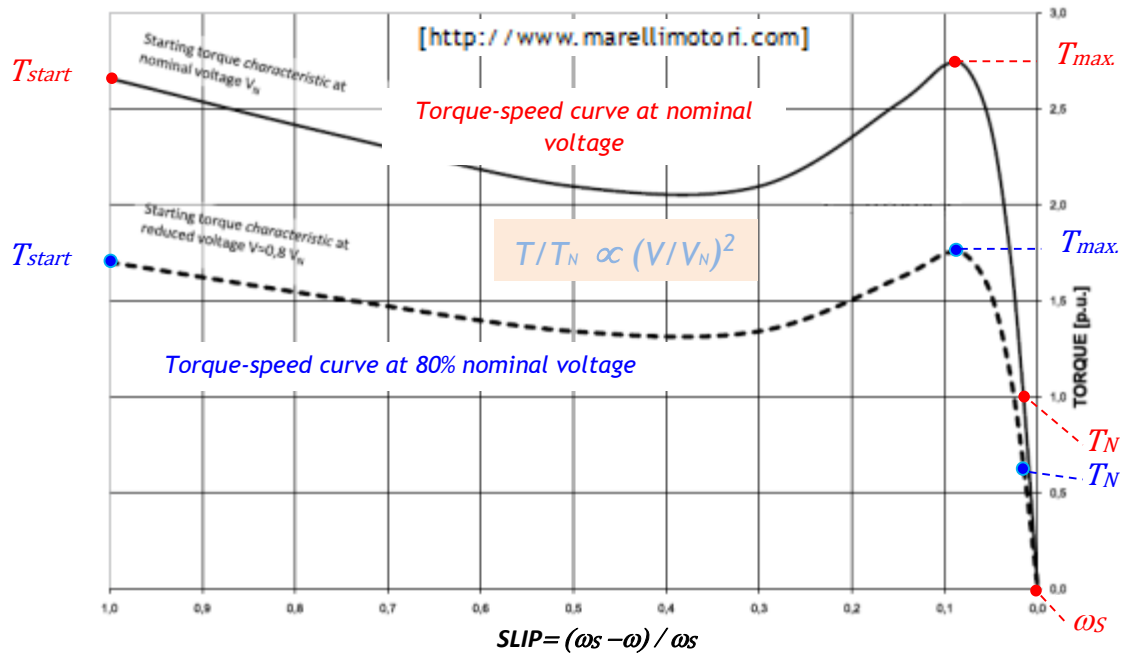
1. Identification of the main components of AC motors: fill in the following figures the designation of the respective component.



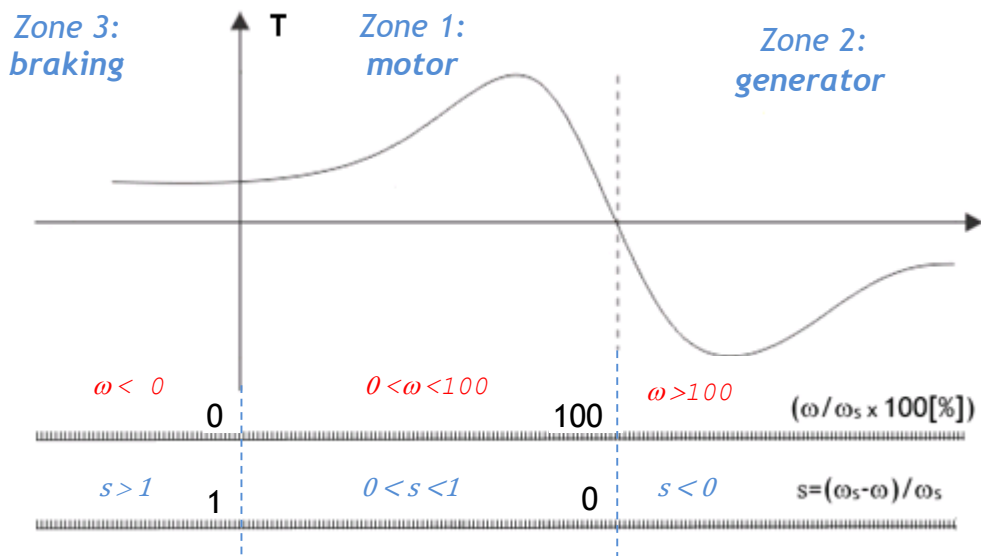
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2. Characteristic curves Torque-speed ( $T, \omega$ )

- a. Identify in the graph below the following ( $T, \omega$ ) working points: nominal, starting, maximum torque and synchronous speed.



- b. In the figure below, it is possible to distinguish three working regions, or zones, of a three-phase induction machine. Considering the different scales for speed (angular speed,  $\omega$ , percent of synchronous speed,  $\% \omega_s$ , slip,  $s$ ) in the horizontal axis, identify these three working zones (1: motor zone; 2: generator zone; 3: braking zone).

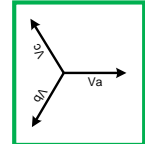


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3. Consider a three-phase power system for an electric motor with a positive, or abc sequence:  $V_a=V_{rms}\angle 0^\circ$ ,  $V_b=V_{rms}\angle -120^\circ$ ,  $V_c=V_{rms}\angle 120^\circ$ . Indicate in the space below the respective: phase and line-to-line voltages, in both the time domain and phasor notation (i.e.  $v_a(t)=V\cos(\omega t+\phi)$ , and  $V_a(j\omega)$ ), considering that  $V_{rms}=230V$ ,  $f=50Hz$ ,  $V_a=V_{L1}$ ,  $V_b=V_{L2}$ ,  $V_c=V_{L3}$ .

**Phase voltages (using rms values in phasors representation)**

$$V_{L1}(j\omega) = V_a(j\omega) = 230\angle 0^\circ [V] \quad V_{L2}(j\omega) = V_b(j\omega) = 230\angle -120^\circ [V] \quad V_{L3}(j\omega) = V_c(j\omega) = 230\angle +120^\circ [V]$$



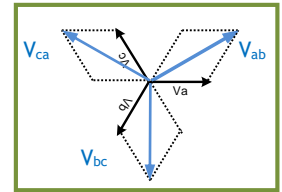
Or, more correctly using angle units coherence:

$$V_{L1}(j\omega) = V_a(j\omega) = 230\angle(0^\circ\pi/180^\circ) [V] \quad V_{L2}(j\omega) = V_b(j\omega) = 230\angle(-120^\circ\pi/180^\circ) [V] \quad V_{L3}(j\omega) = V_c(j\omega) = 230\angle(+120^\circ\pi/180^\circ) [V]$$

$$v_{L1}(t) = 230\sqrt{2} \cos(100\pi t + 0^\circ\pi/180^\circ) [V] \quad v_{L2}(t) = 230\sqrt{2} \cos(100\pi t - 120^\circ\pi/180^\circ) [V] \quad v_{L3}(t) = 230\sqrt{2} \cos(100\pi t + 120^\circ\pi/180^\circ) [V]$$

**Line to line, or compund voltages (using rms values in phasors rep.):**

$$\begin{aligned} V_{12}(j\omega) &= V_{L1}(j\omega) - V_{L2}(j\omega) = 398,4\angle(30^\circ\pi/180^\circ) [V] & v_{12}(t) &= 398,4\sqrt{2} \cos(100\pi t + 30^\circ\pi/180^\circ) [V] \\ V_{23}(j\omega) &= V_{L2}(j\omega) - V_{L3}(j\omega) = 398,4\angle(-90^\circ\pi/180^\circ) [V] & v_{23}(t) &= 398,4\sqrt{2} \cos(100\pi t - 90^\circ\pi/180^\circ) [V] \\ V_{31}(j\omega) &= V_{L3}(j\omega) - V_{L1}(j\omega) = 398,4\angle(+150^\circ\pi/180^\circ) [V] & v_{31}(t) &= 398,4\sqrt{2} \cos(100\pi t + 150^\circ\pi/180^\circ) [V] \end{aligned}$$



**Complex AC power, phasor notation:**  $P(j\omega) = \frac{1}{2}V(j\omega) \cdot I^*(j\omega) = V_{rms}(j\omega) \cdot I_{rms}^*(j\omega)$

$$P_{average, \text{ i.e. real}} = |V_{rms}(j\omega)| \cdot |I_{rms}^*(j\omega)| \cdot \cos \varphi = V_{rms} \cdot I_{rms} \cdot \cos \varphi$$

$$P_{reactive} = |V_{rms}(j\omega)| \cdot |I_{rms}^*(j\omega)| \cdot \sin \varphi = V_{rms} \cdot I_{rms} \cdot \sin \varphi$$

$$P_{apparent} = |V_{rms}(j\omega)| \cdot |I_{rms}^*(j\omega)| = V_{rms} \cdot I_{rms}$$

Power factor:  $\cos \varphi$

$$\text{Phasor impedance: } Z(j\omega) = \frac{V_Z(j\omega)}{I_Z(j\omega)}; |Z(j\omega)| = \frac{|V_Z(j\omega)|}{|I_Z(j\omega)|} = \frac{V_Z}{I_Z}$$

**Star (Y) and delta (Δ) connections:**  $V_{phase}$ ,  $V_{line}$ ,  $I_{line}$ ,  $I_z(\text{load})$ ,  $V_z(\text{load})$ :

$$\text{Delta, } \Delta: I_z = I_{line}/\sqrt{3}; V_z = V_{line-to-line} = V_{phase} \cdot \sqrt{3}$$

$$\text{Star, } \lambda: I_z = I_{line}; V_z = V_{phase}$$

$$\text{Power (real or average)} = 3 \cdot P_z = 3 \cdot V_z \cdot I_z \cdot \cos \varphi$$

Impedance:  $Z_1=Z_2=Z_3 = Z_L$ , balanced three-phase system

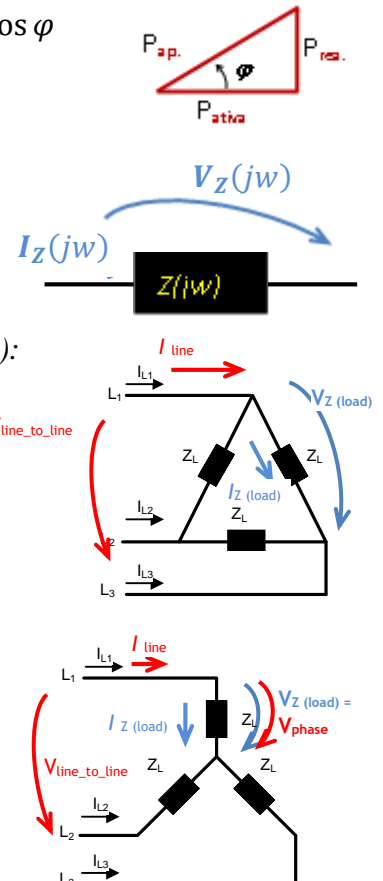
Calculate the following values, as a function of load ( $Z_L$ ):

$$|I_{line\Delta}| = \sqrt{3} \cdot I_z = \sqrt{3} \cdot V_{line\_to\_line} / Z_L$$

$$|I_{line\lambda}| = I_z = V_{phase} / Z_L$$

$$P_\Delta = 3 \cdot P_z = 3 \cdot V_z \cdot I_z \cdot \cos \varphi = 3 \cdot (V_{line\_to\_line})^2 \cdot \cos \varphi / Z_L \quad [W]$$

$$P_\lambda = 3 \cdot P_z = 3 \cdot V_z \cdot I_z \cdot \cos \varphi = 3 \cdot (V_{line\_to\_line} / \sqrt{3})^2 \cdot \cos \varphi / Z_L = P_\Delta / 3 \quad [W]$$



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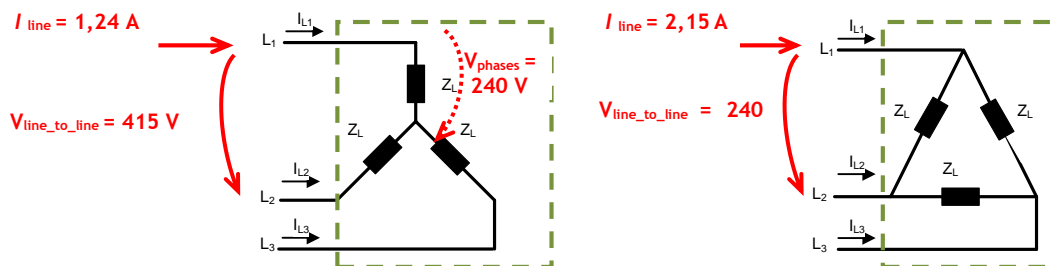
4. Analyze the information included in the plate identification of a three-phase AC induction motor.

| TIPO     |           | M71b4 | N°   | 9716 | Is. Cl. F   | Prot. IP55          | Serv. S1  |
|----------|-----------|-------|------|------|-------------|---------------------|-----------|
| $\Delta$ | $\lambda$ | Hz    | HP   | kW   | n/1'        | A. $\Delta/\lambda$ | $\varphi$ |
| 220/380  | 50        | 0.5   | 0.37 | 1360 | 2.16 / 1.25 | 0.69                |           |
| 240/415  | 50        | 0.5   | 0.37 | 1370 | 2.15 / 1.24 | 0.66                |           |
| 260/440  | 60        | 0.5   | 0.37 | 1630 | 1.83 / 1.06 | 0.69                |           |
| 280/480  | 60        | 0.5   | 0.37 | 1640 | 1.81 / 1.05 | 0.66                |           |

a. Identify from the information of the plate identification the following motor characteristics at 240 $\Delta$ /415 $\lambda$  and 50Hz/:

- frequency /voltage /current: 50 Hz, 240 $\Delta$  or 415 $\lambda$  [V], 2.15 $\Delta$  and 1.24 $\lambda$  [A]
- nominal values of: power 370[W], torque:  $P/\omega = 370/143,5 = 2,58$  Nm speed: 1370 rpm = 143,5 rad/s
- synchronous speed:  $n_s = 1500$  rpm, i.e. the one closest to nominal speed (1370 rpm)
- n° of poles per phase:  $P = 4$ , n° of pairs of poles/phase:  $p = \text{freq (cycles/min)}/ n_s = 3000/1500 = 2$

b. Represent in the figures below the values for supply voltage and current when the motor is connected in star (a) and delta (b) configurations:



c. Considering  $f = 50$  Hz, calculate:

( $\lambda$ )  $P_{active} = 3 \cdot V_{phase} \cdot I_{line} \cdot \cos\phi = 3 \cdot 240 \cdot 1,24 \cdot 0,66 = 589 [W] \cong \sqrt{3} \cdot V_{line\_to\_line} \cdot I_{line} \cdot \cos\phi = \sqrt{3} \cdot 415 \cdot 1,24 \cdot 0,66 = 588 [W]$

( $\Delta$ )  $P_{active} = \sqrt{3} \cdot V_{line\_to\_line} \cdot I_{line} \cdot \cos\phi = \sqrt{3} \cdot 240 \cdot 2,15 \cdot 0,66 = 589 [W]$

( $\lambda$ )  $P_{reactive} = 3 \cdot V_{phase} \cdot I_{line} \cdot \sin\phi = 3 \cdot 240 \cdot 1,24 \cdot 0,75 = 670 [VAR]$

( $\Delta$ )  $P_{reactive} = \sqrt{3} \cdot V_{line\_to\_line} \cdot I_{line} \cdot \sin\phi = \sqrt{3} \cdot 240 \cdot 2,15 \cdot 0,75 = 670 [VAR]$

$P_{apparent} = P_{active} / \cos\phi = 589 / \cos\phi = 892 [VA]$

d. Estimate the efficiency of the motor and compare the value with an equivalent motor (i.e. M71B4 da Carpanelli, in the available pdf documents:  $\eta_{motor} = 65 \%$ )

e. What motor connection ( $\Delta$  or  $\lambda$ ) to use if the motor is to be powered directly (DOL) from the AI laboratory electric installation? star ( $\lambda$ ).

